

9.5. Regulator design

Typical specifications:

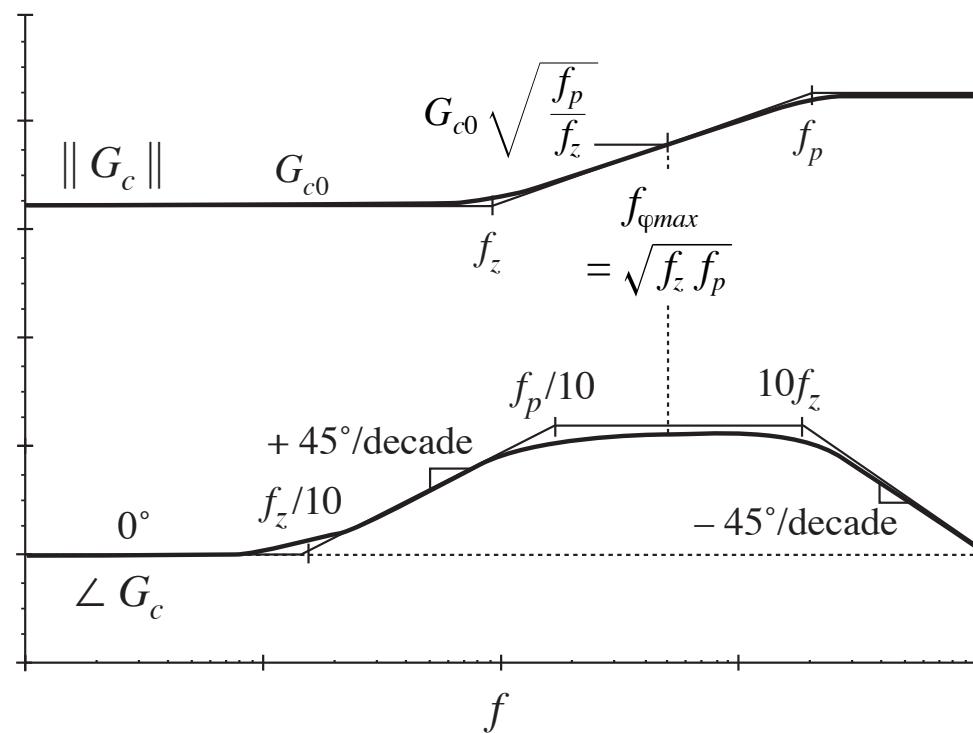
- Effect of load current variations on output voltage regulation
This is a limit on the maximum allowable output impedance
- Effect of input voltage variations on the output voltage regulation
This limits the maximum allowable line-to-output transfer function
- Transient response time
This requires a sufficiently high crossover frequency
- Overshoot and ringing
An adequate phase margin must be obtained

The regulator design problem: add compensator network $G_c(s)$ to modify $T(s)$ such that all specifications are met.

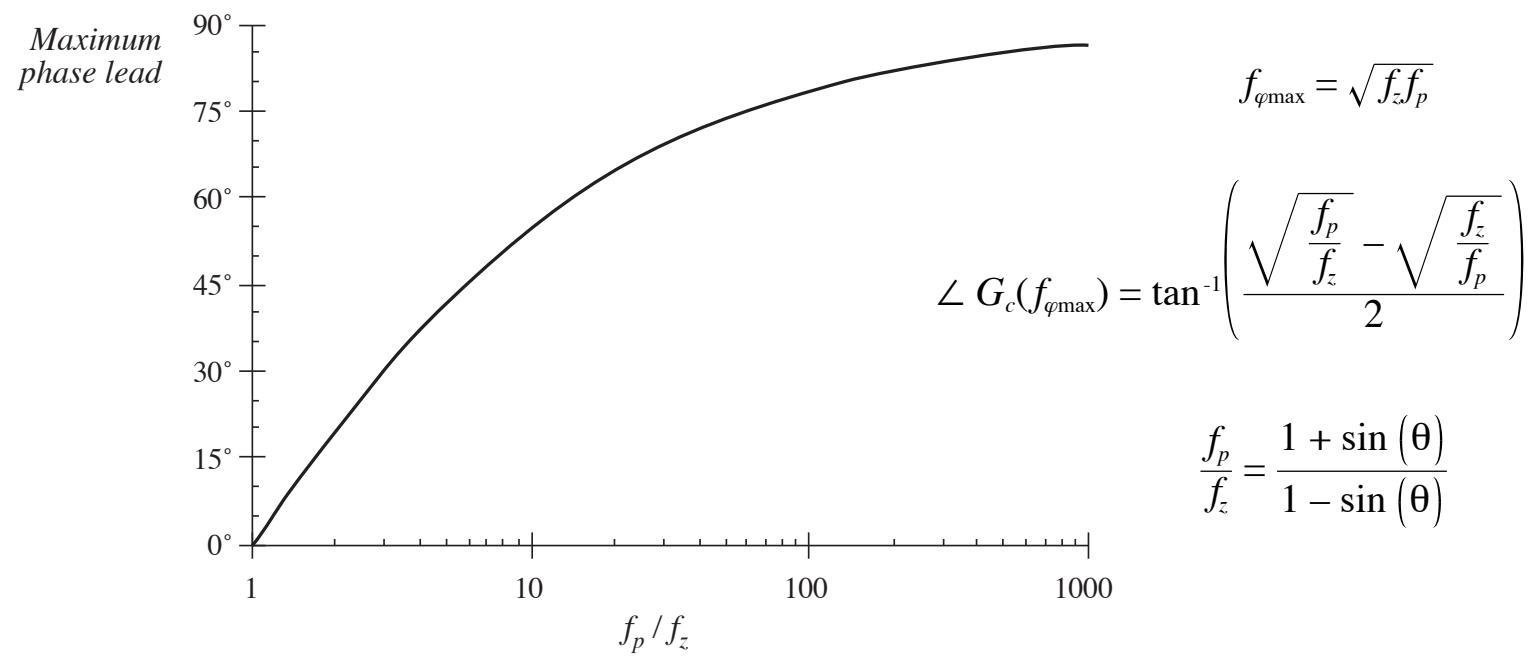
9.5.1. Lead (PD) compensator

$$G_c(s) = G_{c0} \frac{\left(1 + \frac{s}{\omega_z}\right)}{\left(1 + \frac{s}{\omega_p}\right)}$$

Improves phase margin



Lead compensator: maximum phase lead



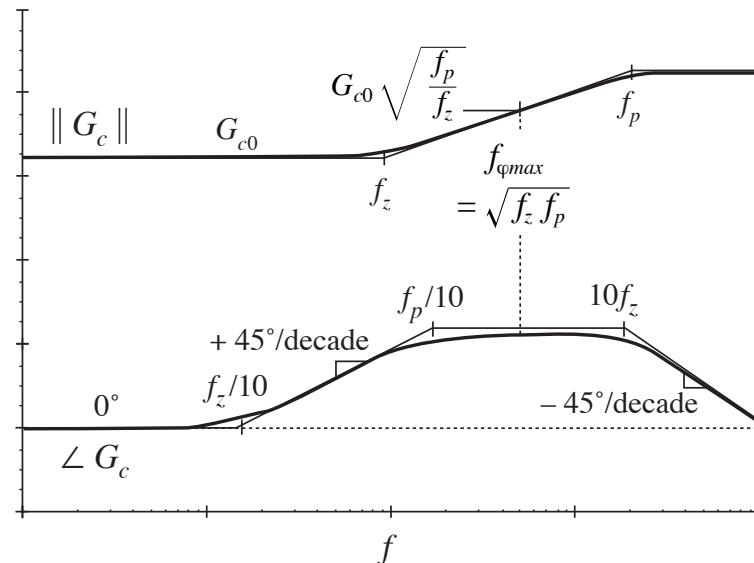
Lead compensator design

To optimally obtain a compensator phase lead of θ at frequency f_c , the pole and zero frequencies should be chosen as follows:

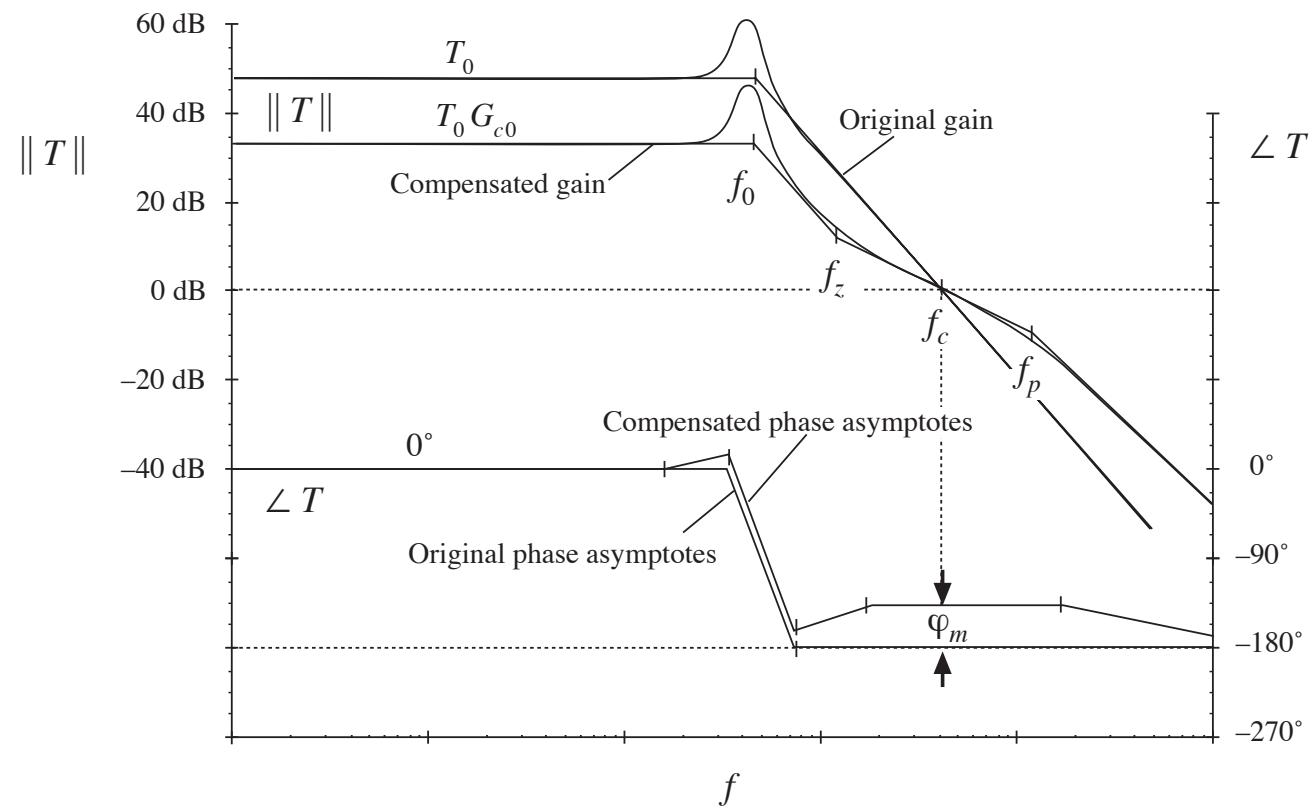
$$f_z = f_c \sqrt{\frac{1 - \sin(\theta)}{1 + \sin(\theta)}}$$
$$f_p = f_c \sqrt{\frac{1 + \sin(\theta)}{1 - \sin(\theta)}}$$

If it is desired that the magnitude of the compensator gain at f_c be unity, then G_{c0} should be chosen as

$$G_{c0} = \sqrt{\frac{f_z}{f_p}}$$



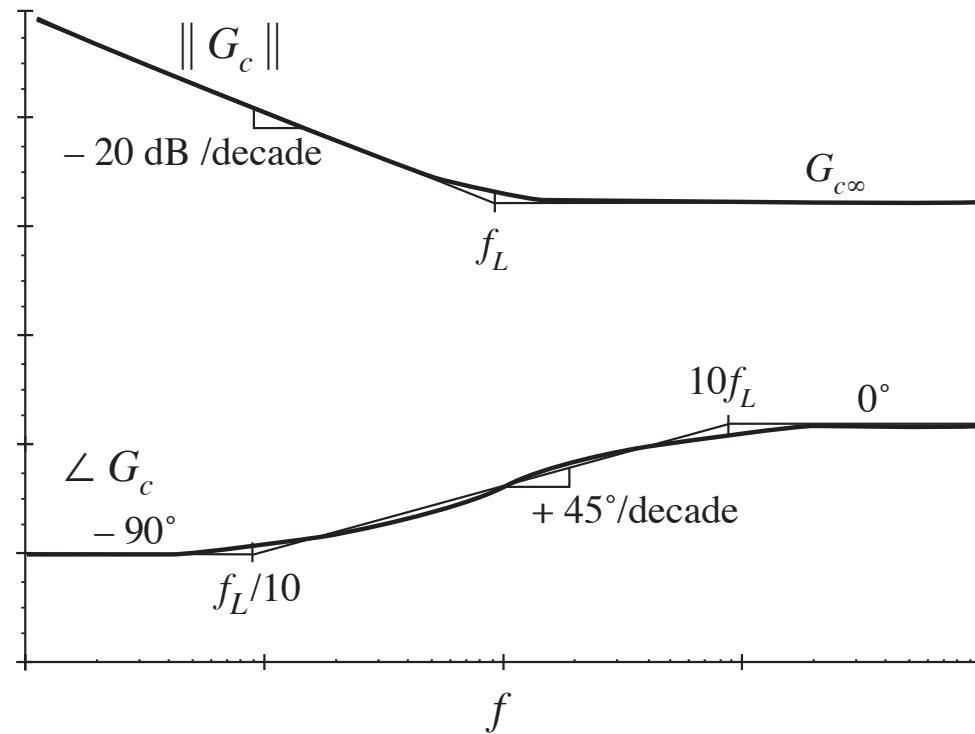
Example: lead compensation



9.5.2. Lag (PI) compensation

$$G_c(s) = G_{c\infty} \left(1 + \frac{\omega_L}{s} \right)$$

Improves low-frequency loop gain and regulation



Example: lag compensation

original
(uncompensated)
loop gain is

$$T_u(s) = \frac{T_{u0}}{\left(1 + \frac{s}{\omega_0}\right)}$$

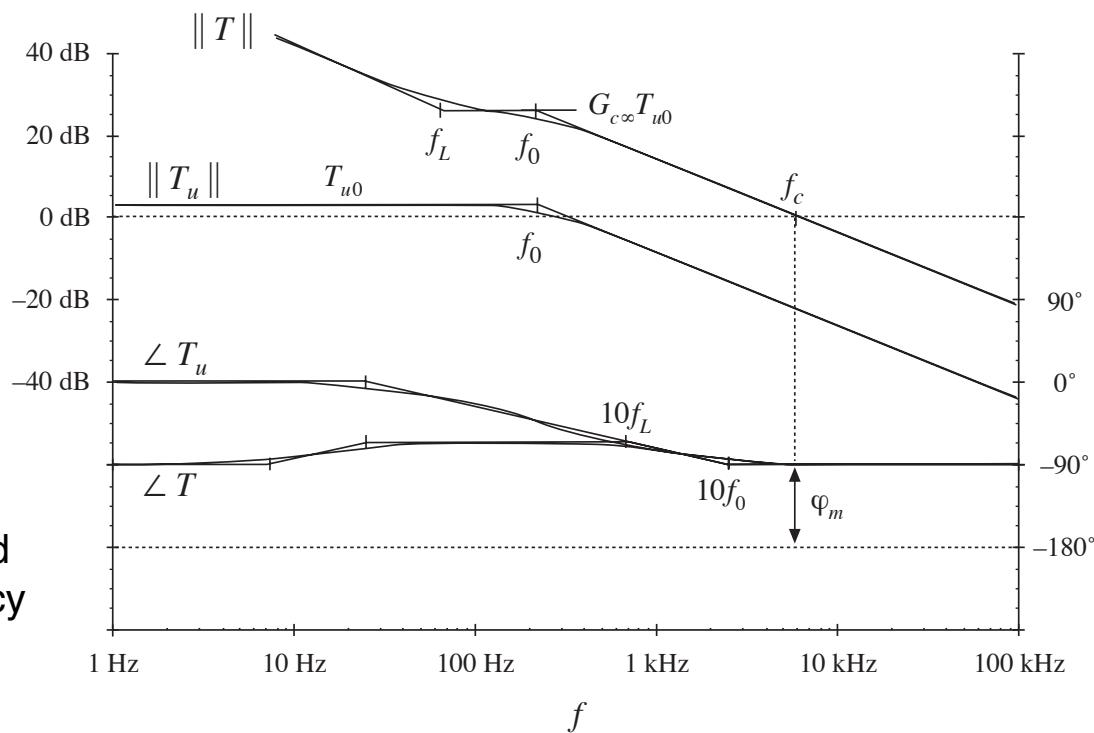
compensator:

$$G_c(s) = G_{c\infty} \left(1 + \frac{\omega_L}{s}\right)$$

Design strategy:
choose

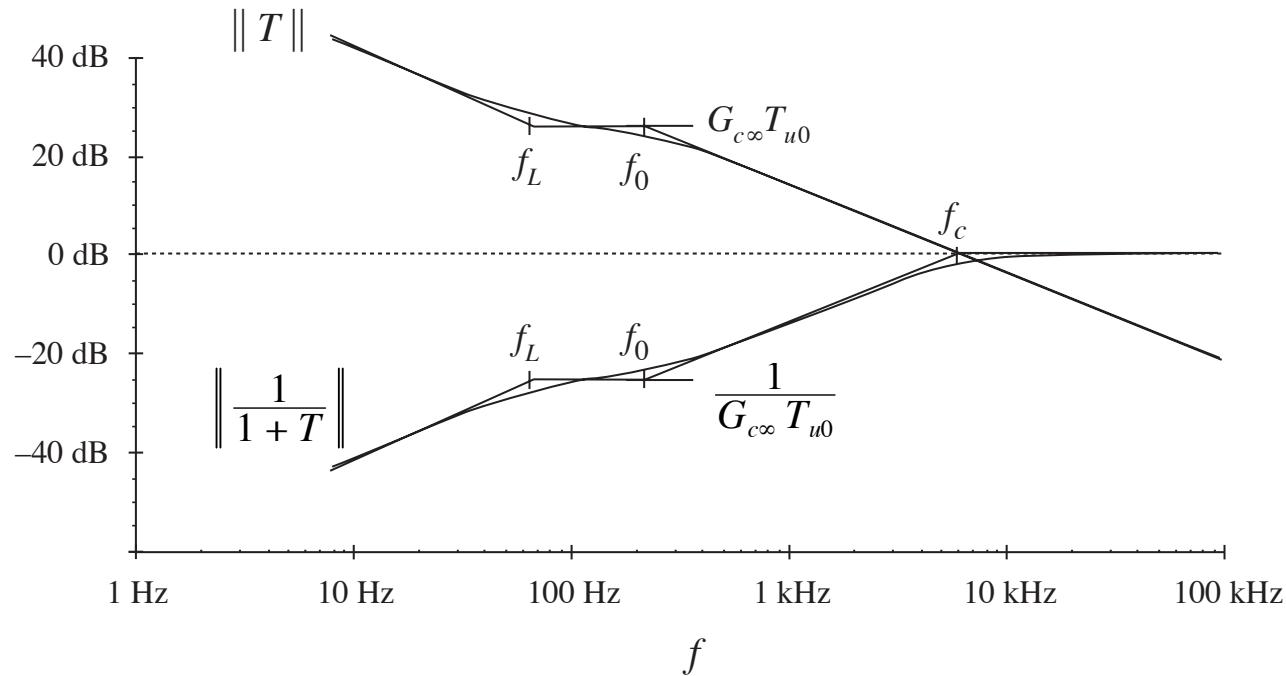
$G_{c\infty}$ to obtain desired
crossover frequency

ω_L sufficiently low to
maintain adequate
phase margin



Example, continued

Construction of $1/(1+T)$, lag compensator example:



9.5.3. Combined (PID) compensator

