

## 7.5 The canonical circuit model

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All PWM CCM dc-dc converters perform the same basic functions:

- Transformation of voltage and current levels, ideally with 100% efficiency
- Low-pass filtering of waveforms
- Control of waveforms by variation of duty cycle

Hence, we expect their equivalent circuit models to be qualitatively similar.

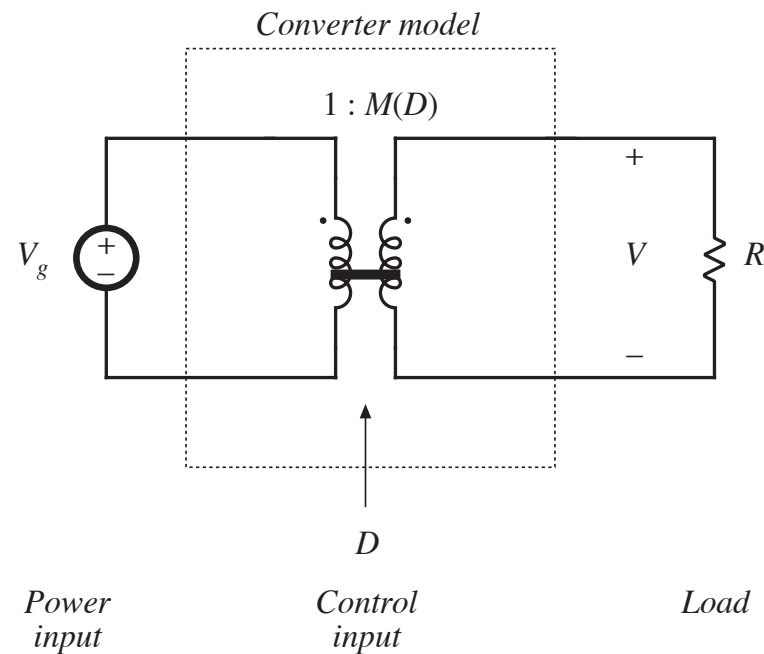
Canonical model:

- A standard form of equivalent circuit model, which represents the above physical properties
- Plug in parameter values for a given specific converter

## 7.5.1. Development of the canonical circuit model

### 1. Transformation of dc voltage and current levels

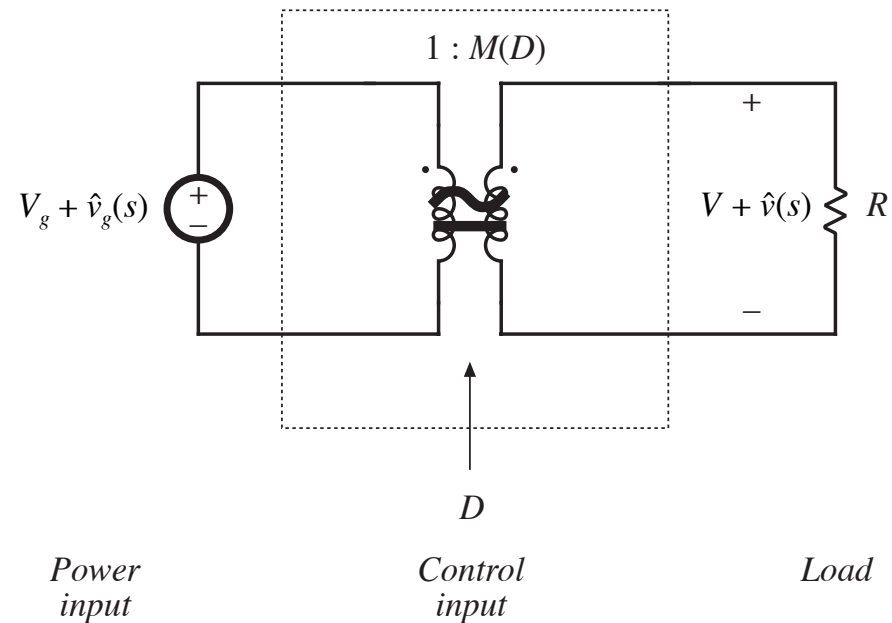
- modeled as in Chapter 3 with ideal dc transformer
- effective turns ratio  $M(D)$
- can refine dc model by addition of effective loss elements, as in Chapter 3



## Steps in the development of the canonical circuit model

2. Ac variations in  $v_g(t)$  induce ac variations in  $v(t)$

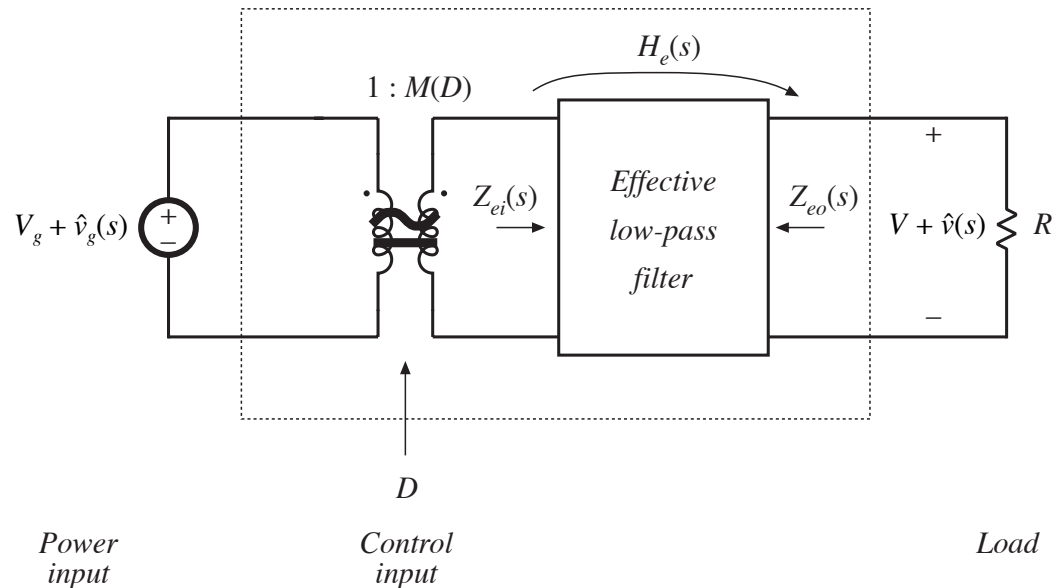
- these variations are also transformed by the conversion ratio  $M(D)$



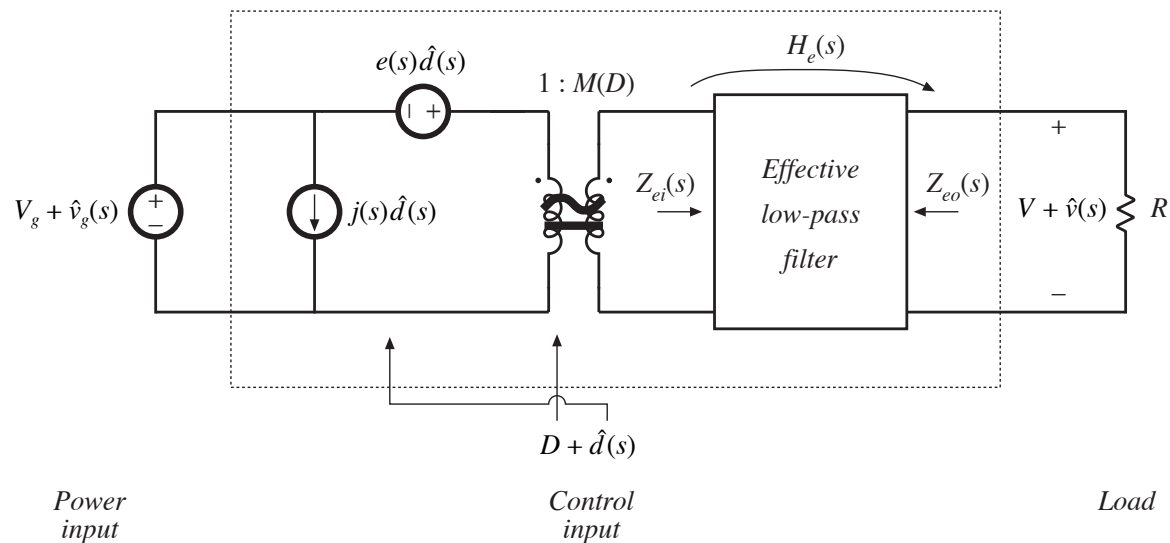
## Steps in the development of the canonical circuit model

3. Converter must contain an effective low-pass filter characteristic

- necessary to filter switching ripple
- also filters ac variations
- effective filter elements may not coincide with actual element values, but can also depend on operating point

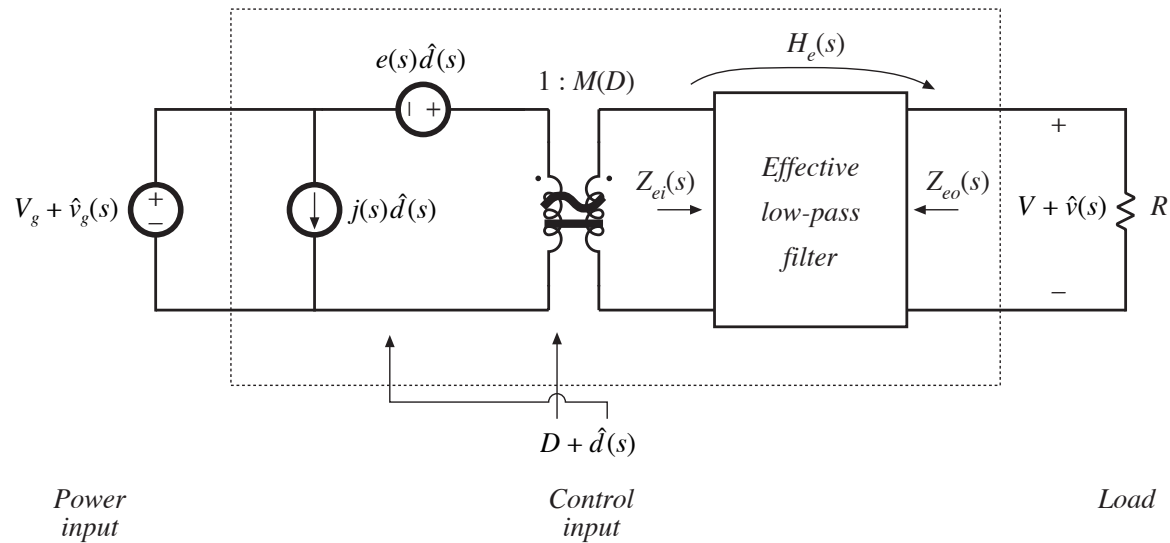


## Steps in the development of the canonical circuit model



4. Control input variations also induce ac variations in converter waveforms
  - Independent sources represent effects of variations in duty cycle
  - Can push all sources to input side as shown. Sources may then become frequency-dependent

## Transfer functions predicted by canonical model

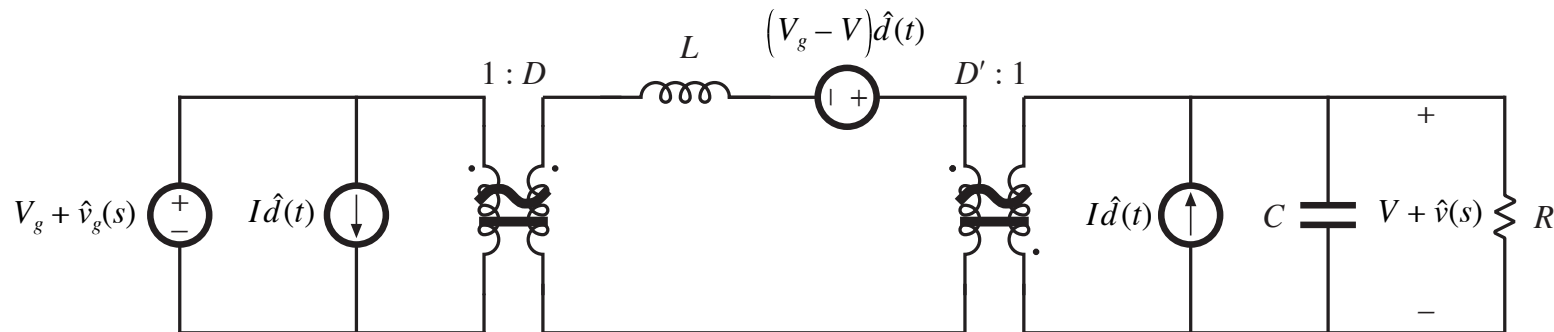


Line-to-output transfer function: 
$$G_{vg}(s) = \frac{\hat{v}(s)}{\hat{v}_g(s)} = M(D) H_e(s)$$

Control-to-output transfer function: 
$$G_{vd}(s) = \frac{\hat{v}(s)}{\hat{d}(s)} = e(s) M(D) H_e(s)$$

## 7.5.2 Example: manipulation of the buck-boost converter model into canonical form

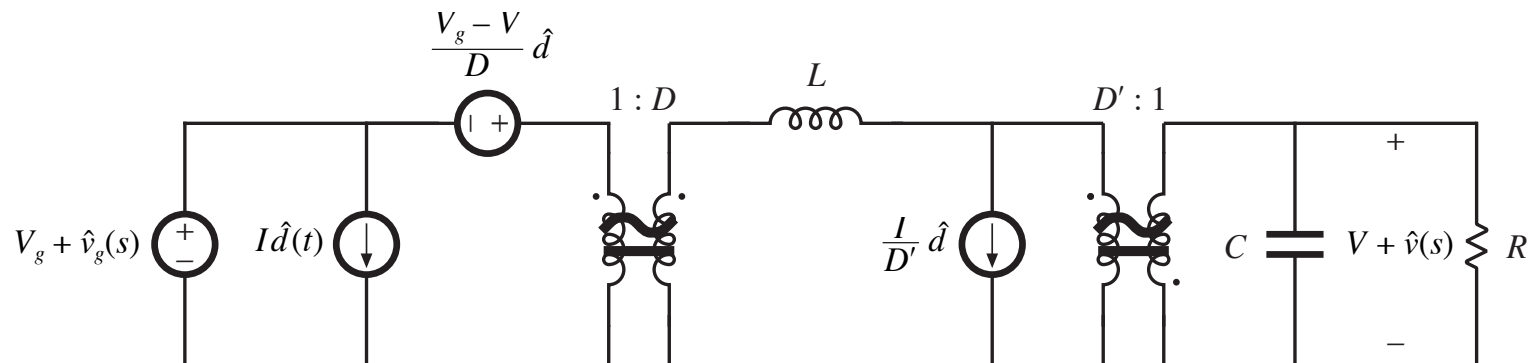
*Small-signal ac model of the buck-boost converter*



- Push independent sources to input side of transformers
- Push inductor to output side of transformers
- Combine transformers

# Step 1

- Push voltage source through  $1:D$  transformer
- Move current source through  $D':1$  transformer



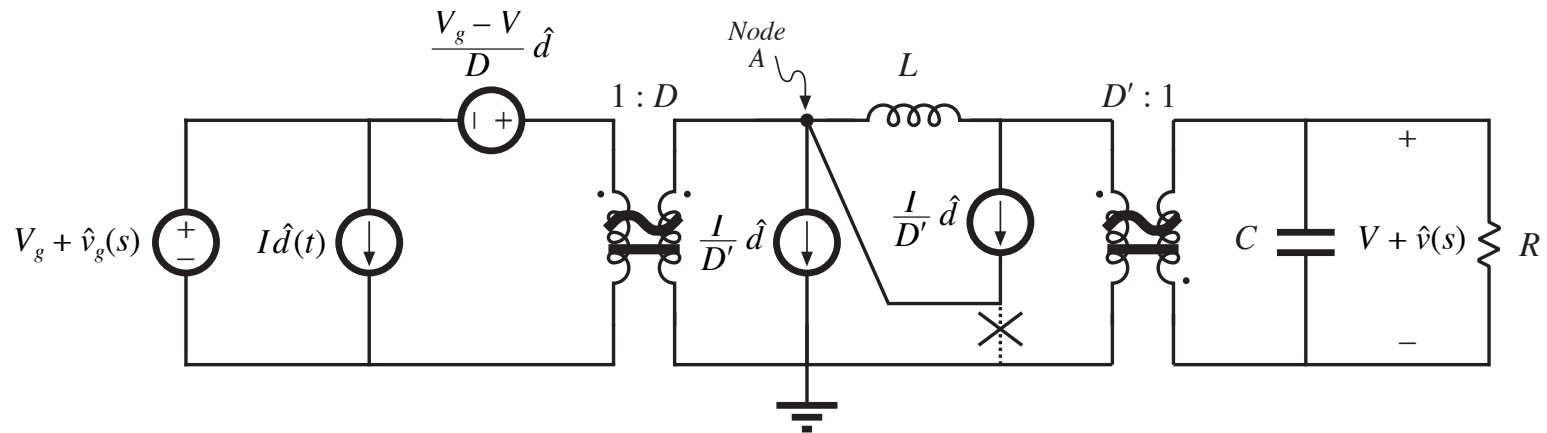


## Step 2

How to move the current source past the inductor:

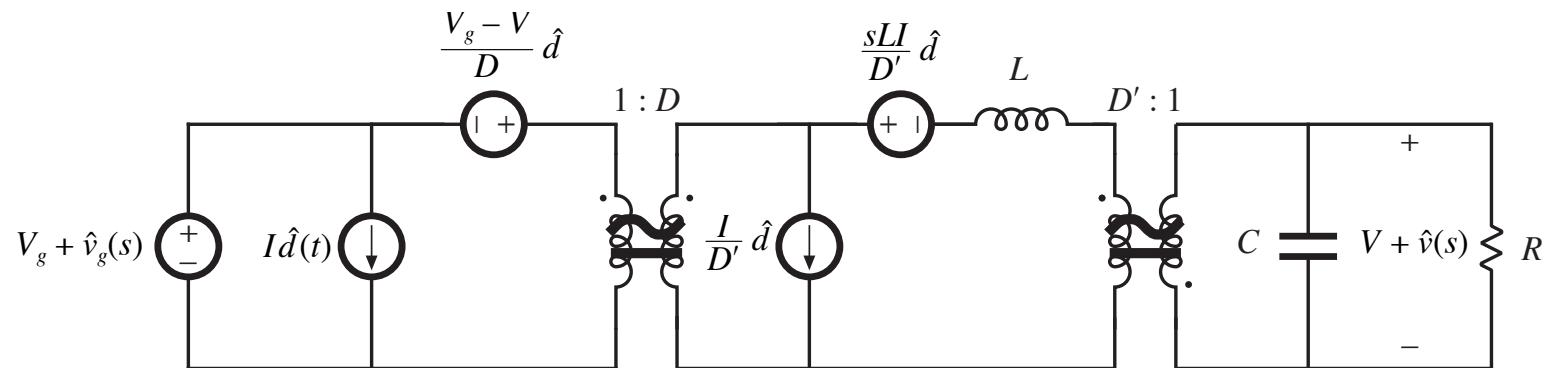
Break ground connection of current source, and connect to node A instead.

Connect an identical current source from node A to ground, so that the node equations are unchanged.



## Step 3

The parallel-connected current source and inductor can now be replaced by a Thevenin-equivalent network:



## Step 4

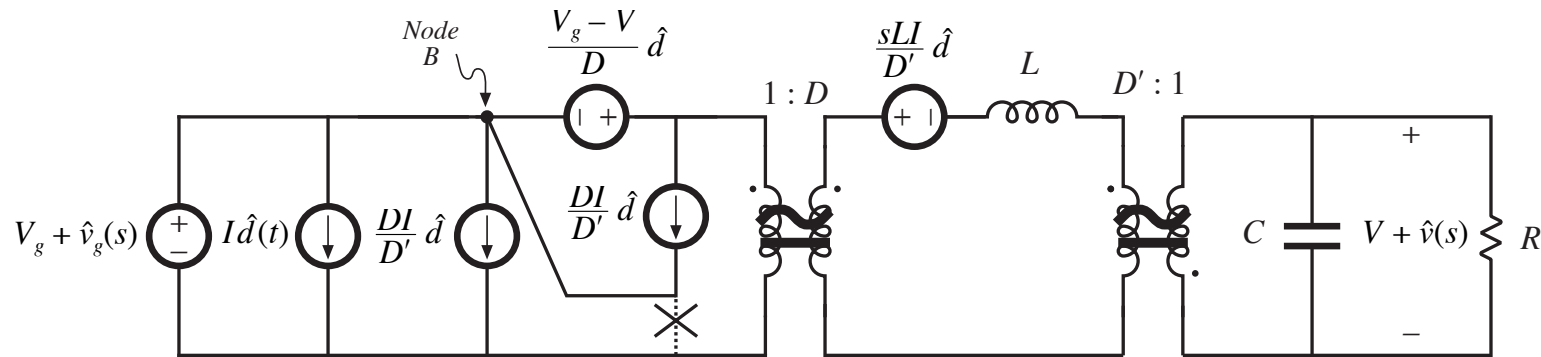
Now push current source through 1: $D$  transformer.

Push current source past voltage source, again by:

Breaking ground connection of current source, and connecting to node  $B$  instead.

Connecting an identical current source from node  $B$  to ground, so that the node equations are unchanged.

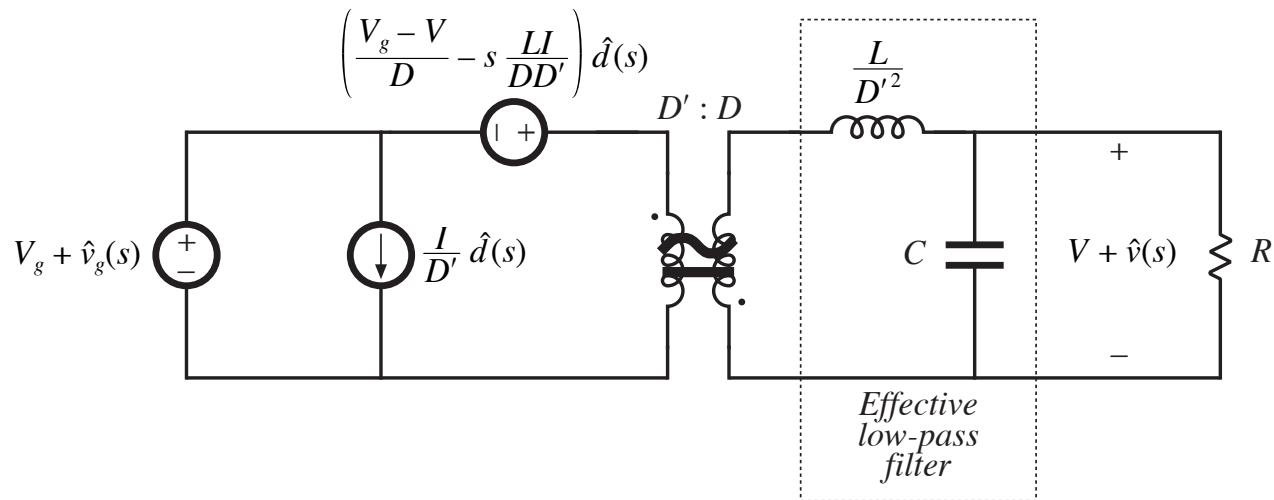
Note that the resulting parallel-connected voltage and current sources are equivalent to a single voltage source.



## Step 5: final result

Push voltage source through 1:D transformer, and combine with existing input-side transformer.

Combine series-connected transformers.



## Coefficient of control-input voltage generator

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Voltage source coefficient is:

$$e(s) = \frac{V_g + V}{D} - \frac{sLI}{D D'}$$

Simplification, using dc relations, leads to

$$e(s) = -\frac{V}{D^2} \left( 1 - \frac{sDL}{D'^2 R} \right)$$

Pushing the sources past the inductor causes the generator to become frequency-dependent.

## 7.5.3 Canonical circuit parameters for some common converters

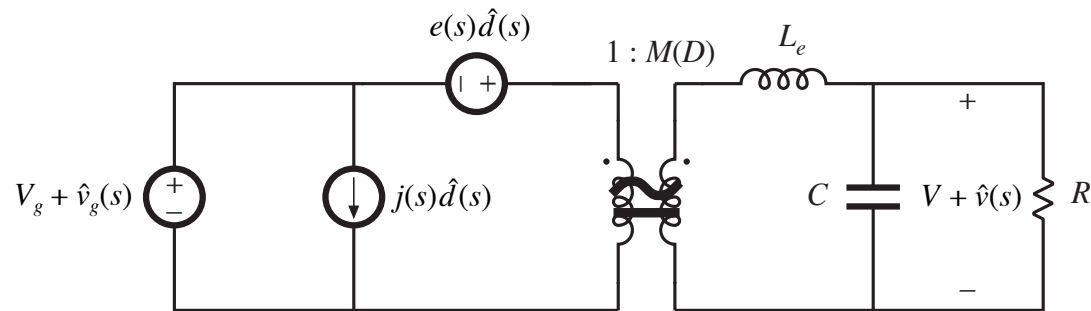


Table 7.1. Canonical model parameters for the ideal buck, boost, and buck-boost converters

Converter	$M(D)$	$L_e$	$e(s)$	$j(s)$
Buck	$D$	$L$	$\frac{V}{D^2}$	$\frac{V}{R}$
Boost	$\frac{1}{D}$	$\frac{L}{D^2}$	$V \left(1 - \frac{sL}{D^2 R}\right)$	$\frac{V}{D^2 R}$
Buck-boost	$-\frac{D}{D'}$	$\frac{L}{D'^2}$	$-\frac{V}{D^2} \left(1 - \frac{sDL}{D'^2 R}\right)$	$-\frac{V}{D'^2 R}$