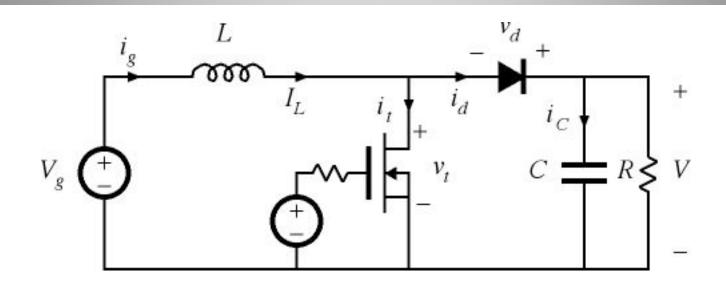
### Boost Converter Example

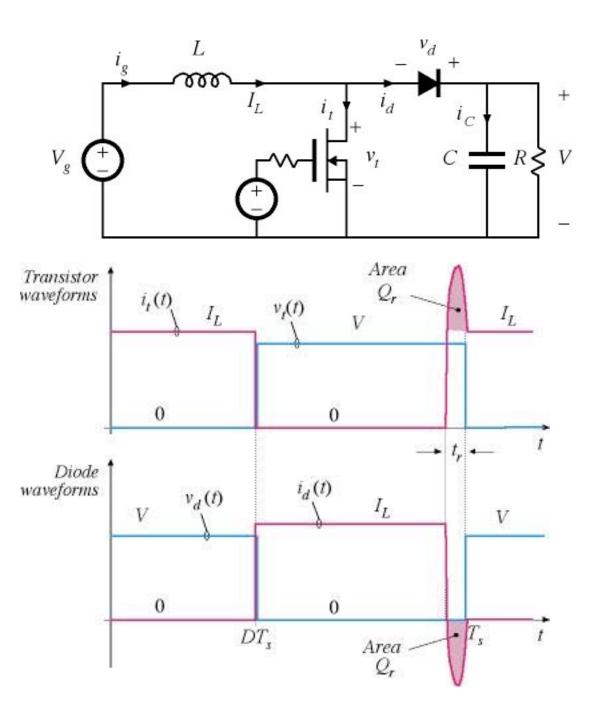


Model same effects as in previous buck converter example:

- Ideal MOSFET, *p*–*n* diode with reverse recovery
- Neglect semiconductor device capacitances, MOSFET switching times, etc.
- Neglect conduction losses
- Neglect ripple in inductor current and capacitor voltage

# Boost converter

Transistor and diode waveforms have same shapes as in buck example, but depend on different quantities



## Inductor volt-second balance and average input current

$$v_{L}(t) \uparrow V_{g}$$

$$\leftarrow DT_{s} \longrightarrow D'T_{s} \longrightarrow$$

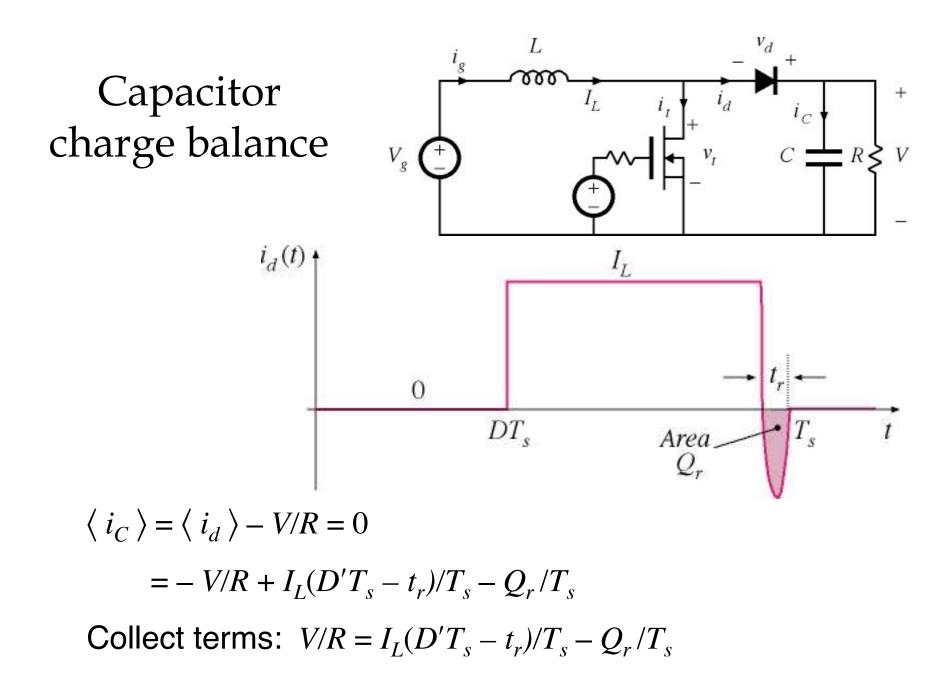
$$V_{g} - V$$

$$t$$

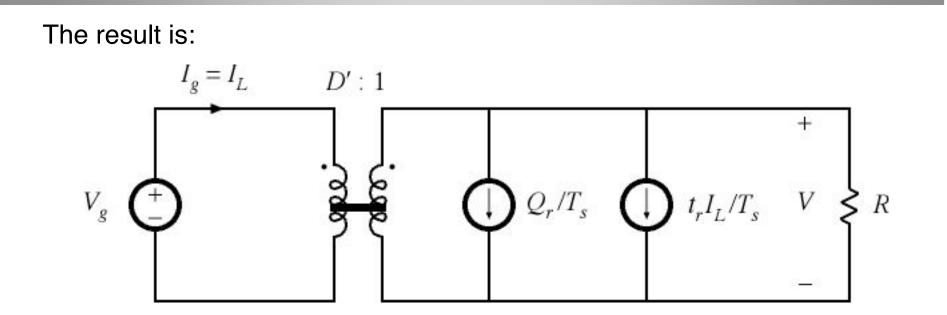
$$v_{L}(t) = V_{g} - v_{t}(t)$$

As usual:  $\langle v_L \rangle = 0 = V_g - D'V$ 

Also as usual:  $\langle i_g \rangle = I_L$ 



#### Construct model



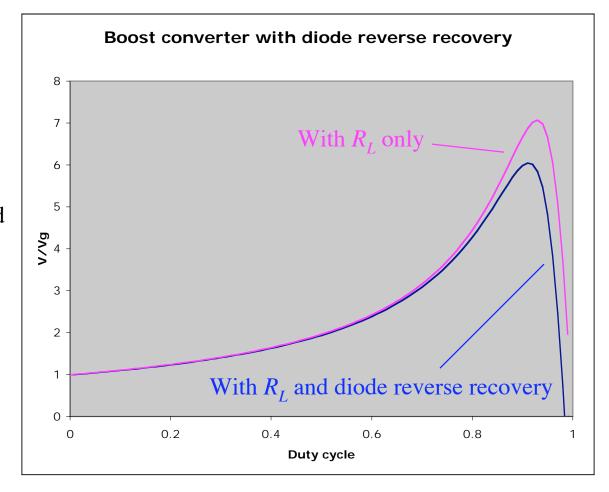
The two independent current sources consume power

 $V\left(t_r I_L / T_s + Q_r / T_s\right)$ 

equal to the switching loss induced by diode reverse recovery

## Predicted $V/V_g$ vs duty cycle

Switching frequency 100 kHz Input voltage 24 V Load resistance 60  $\Omega$ Recovered charge 5  $\mu$ Coul Reverse recovery time 100 nsec Inductor resistance  $R_L = 0.3 \Omega$ (inductor resistance also inserted into averaged model here)



## Summary

The averaged modeling approach can be extended to include effects of switching loss

- Transistor and diode waveforms are constructed, including the switching transitions. The effects of the switching transitions on the inductor, capacitor, and input current waveforms can then be determined
- Inductor volt-second balance and capacitor charge balance are applied
- Converter input current is averaged
- Equivalent circuit corresponding to the the averaged equations is constructed